

# PBW 620 Advanced Soil Mechanics II

# PBW 584 Applied Soil Mechanics

Public Works Department

MSc. Degree

Spring Semester

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Soil Mechanics and Foundations Research Lab

Faculty of Engineering- Cairo University

Part II



- APPLICATION OF  
NUMERICAL METHODS  
IN BEARING CAPACITY  
PROBLEM**
- EARTH PRESSURE**

# Acknowledgment

- Finite Element Modeling in Geotechnical Engineering (Potts and Zdravkovic)
- Dr. C. M. Martin University of Oxford
- Prof. Andrew Whittle lecture notes, Massachusetts Institute of Technology
- Prof. Dr. Hani Lotfi

# Outline of Part II

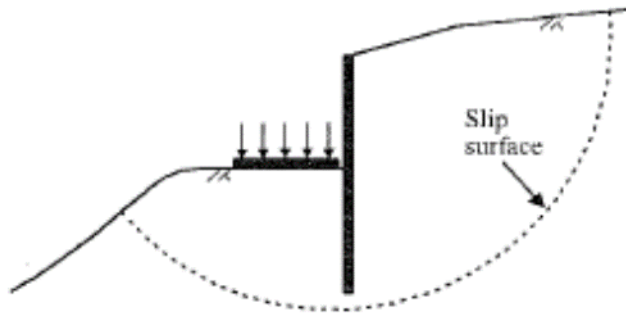
Lecture	Description
First	Comparison between numerical methods and conventional Methods of Analysis
Second	Application of Analytical and Numerical methods to the Bearing Capacity Problem
Third	Earth Pressure using conventional analysis
Fourth	Special Conditions affecting earth pressure in design - Part I
Fifth	Special Conditions affecting earth pressure in design – Part 2

# Lecture I Outline

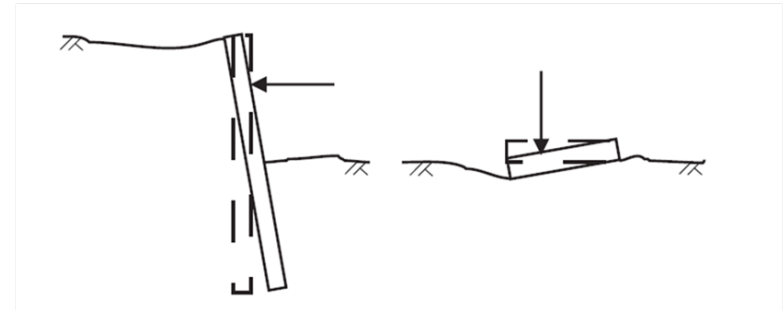
- Geotechnical Analysis Framework
- What are the conventional methods
- What are the numerical methods
- Comparisons and Discussion

# Geotechnical Eng. Problem

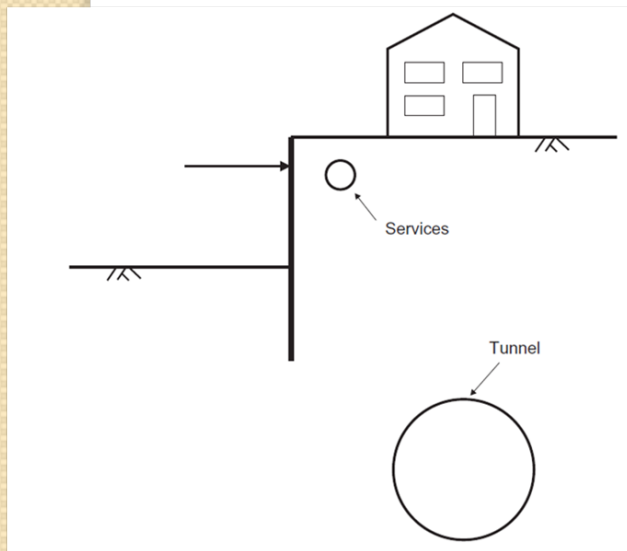
## Stability



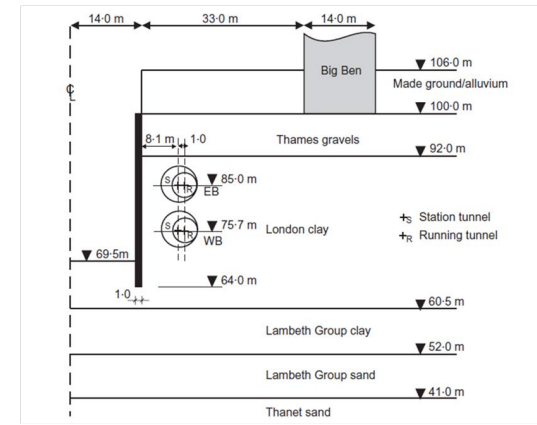
## Deformations



## Movement



## Adjacent Structures



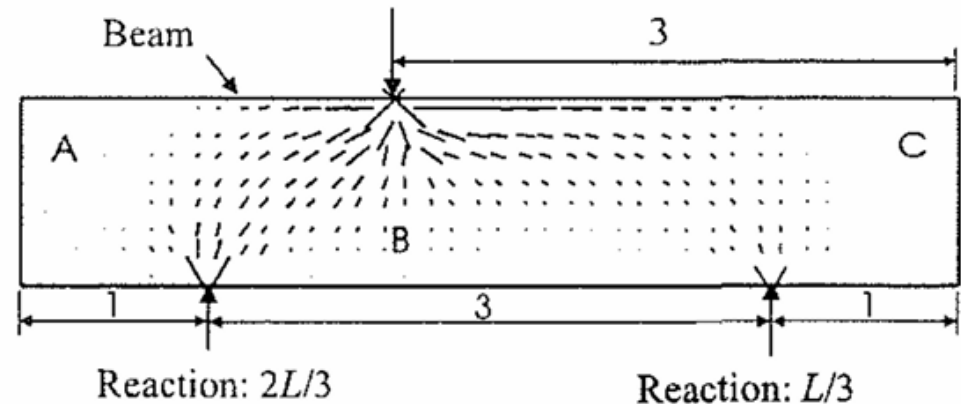
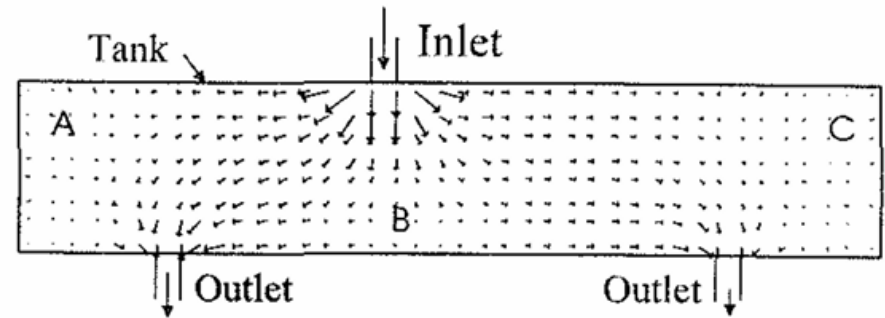
# Analysis Framework

## I- Equilibrium

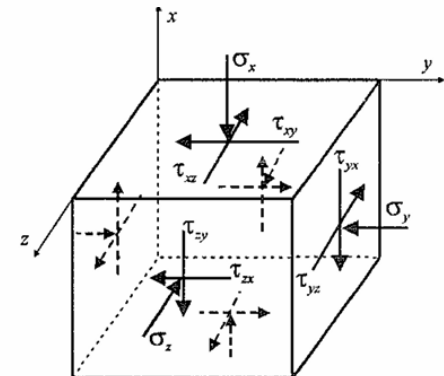
$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + \gamma = 0$$

$$\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} = 0$$

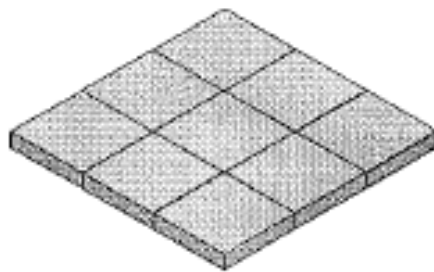
$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_z}{\partial z} = 0$$



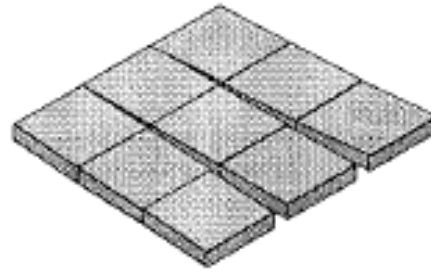
- Force Boundary Conditions
- Displacement Boundary Conditions



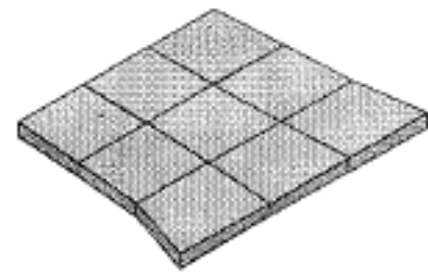
# II-Compatibility



a) Original



b) Non-compatible



c) Compatible

$$\epsilon_x = -\frac{\partial u}{\partial x} ; \epsilon_y = -\frac{\partial v}{\partial y} ; \epsilon_z = -\frac{\partial w}{\partial z}$$

$$\gamma_{xy} = -\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} ; \gamma_{yz} = -\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} ; \gamma_{xz} = -\frac{\partial w}{\partial x} - \frac{\partial u}{\partial z}$$

# III-Constitutive Models

$$\begin{Bmatrix} \Delta\sigma_x \\ \Delta\sigma_y \\ \Delta\sigma_z \\ \Delta\tau_{xy} \\ \Delta\tau_{xz} \\ \Delta\tau_{zy} \end{Bmatrix} = \begin{bmatrix} D_{11} & D_{12} & D_{13} & D_{14} & D_{15} & D_{16} \\ D_{21} & D_{22} & D_{23} & D_{24} & D_{25} & D_{26} \\ D_{31} & D_{32} & D_{33} & D_{34} & D_{35} & D_{36} \\ D_{41} & D_{42} & D_{43} & D_{44} & D_{45} & D_{46} \\ D_{51} & D_{52} & D_{53} & D_{54} & D_{55} & D_{56} \\ D_{61} & D_{62} & D_{63} & D_{64} & D_{65} & D_{66} \end{bmatrix} \begin{Bmatrix} \Delta\varepsilon_x \\ \Delta\varepsilon_y \\ \Delta\varepsilon_z \\ \Delta\gamma_{xy} \\ \Delta\gamma_{xz} \\ \Delta\gamma_{zy} \end{Bmatrix}$$

# Methods of Analysis

```
graph TD; A[Methods of Analysis] --> B[Conventional Methods]; A --> C[Numerical Analysis]
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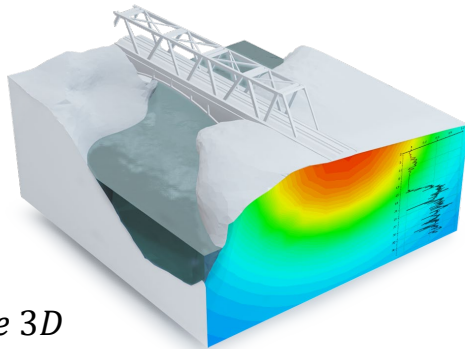
Conventional  
Methods

Numerical  
Analysis

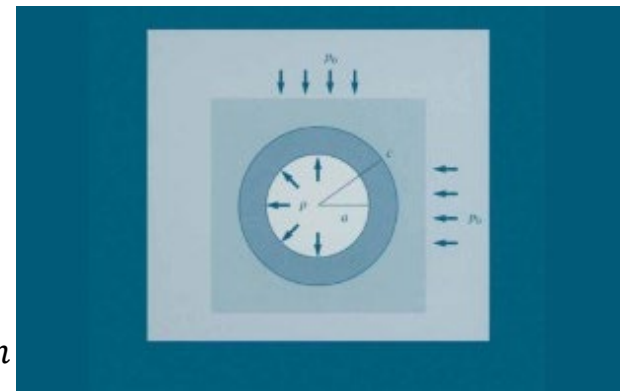
# Conventional Methods

## Closed Form

- The solution is exact in a theoretical sense but is still an approximation to the real problem.
- Soil behaves in an isotropic linear-elastic manner.
- Practical application is limited to cases with geometric symmetries.



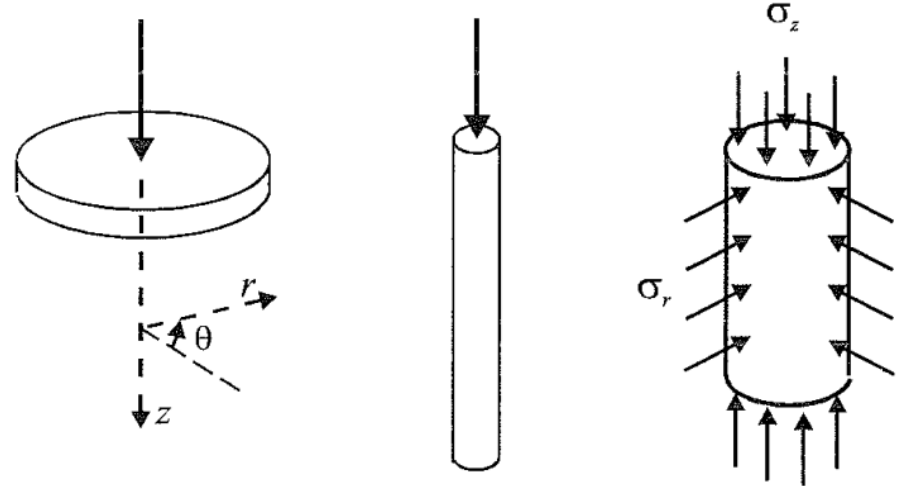
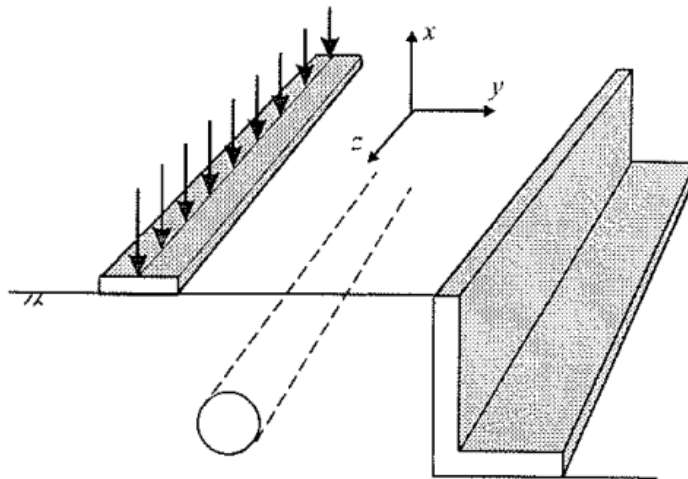
*Settle 3D*



*Cavity Expansion*

# Geometric Idealization

Plane Strain Conditions

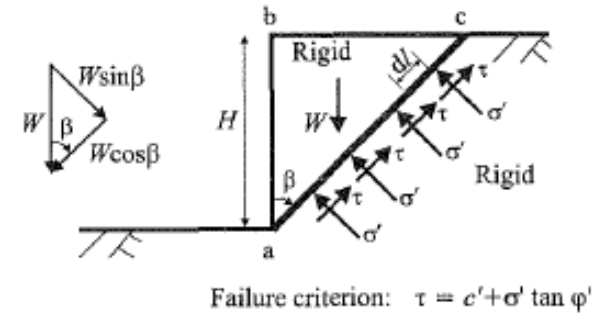


Axisymmetric Conditions

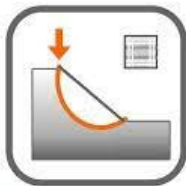
# Conventional methods: Simple methods

## Limit Equilibrium

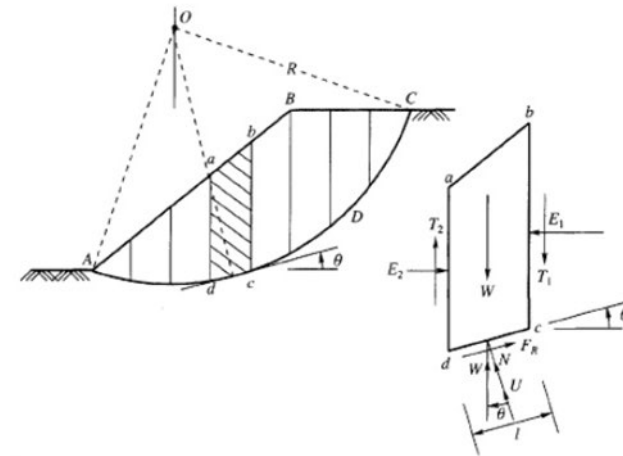
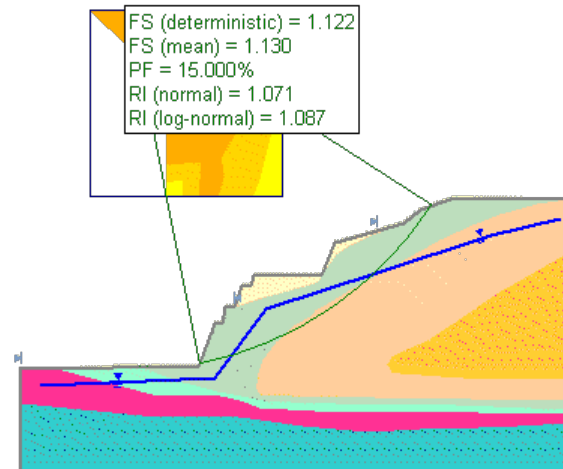
- Coulomb's earth pressure
- Method of Slices



Slide



TOPO SCIENCE  
RAHIM SOFTWARES



# Conventional methods: Simple methods

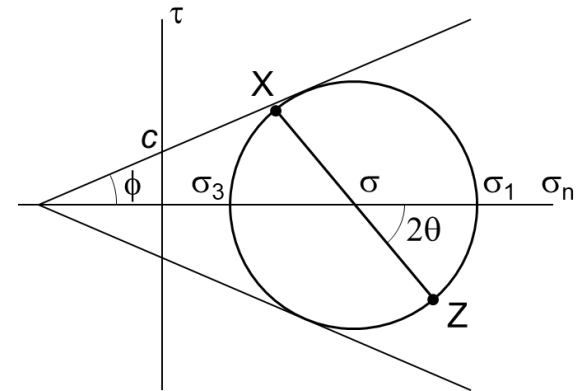
## Stress Fields

- Rankine Earth Pressure
- Bearing Capacity

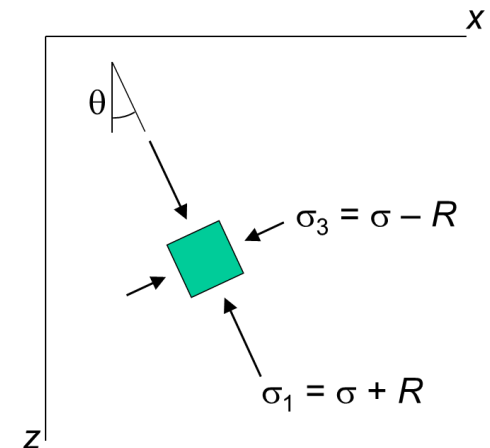
Solving Equilibrium differential Equations with a failure criterion to solve for stresses every where

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \tau_{xz}}{\partial z} = 0$$

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \sigma_{zz}}{\partial z} = \gamma$$



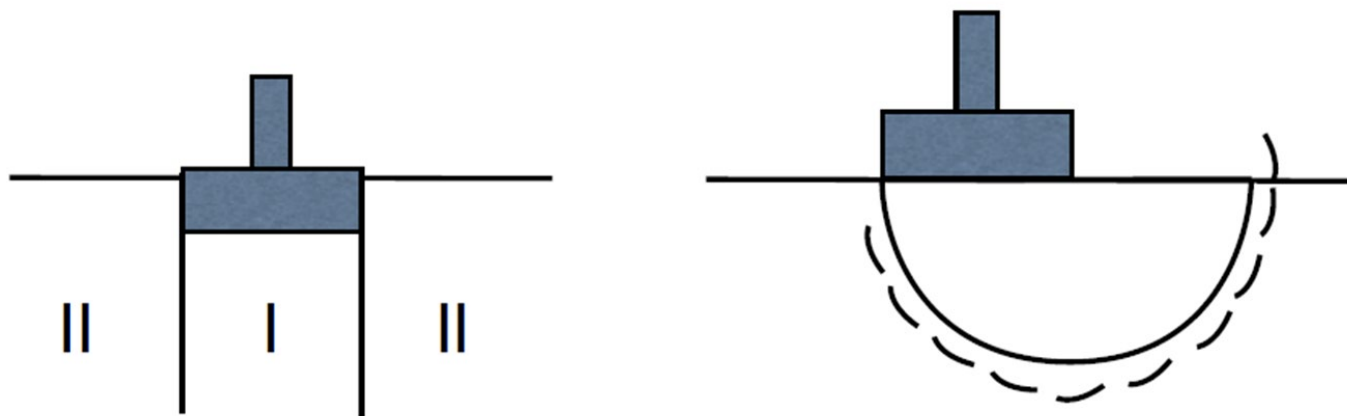
$$R = c \cos \phi + \sigma \sin \phi$$



# Conventional methods: Simple methods

## Limit Analysis

The true solution of a problem lies between an upper bound which is an unsafe solution (ignores equilibrium) and a lower bound which is a too conservative solution (ignores compatibility)



# Lower Bound Theorem

If a distribution of stresses can be found within the body which satisfies equilibrium at all points in the body and does not exceed yield criteria then exterior loads are lower bound loads to the true collapse loading conditions.

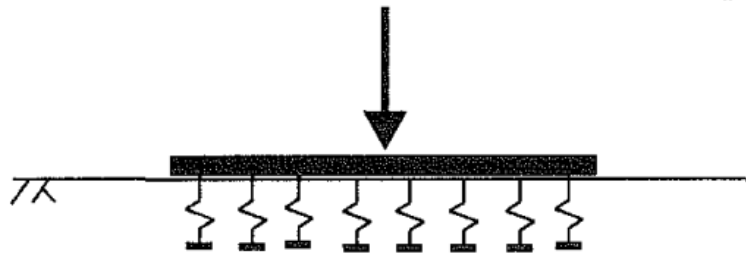
This is actually what we need: A Design value for the external loads that will always be less than the true collapse value

# Upper Bound Theorem

If a distribution of velocity field (a mechanism of failure) can be found such that the rate of work done by the externally applied loads is larger than the energy dissipated internally by the material then exterior loads are upper bound loads to the true collapse loading conditions.

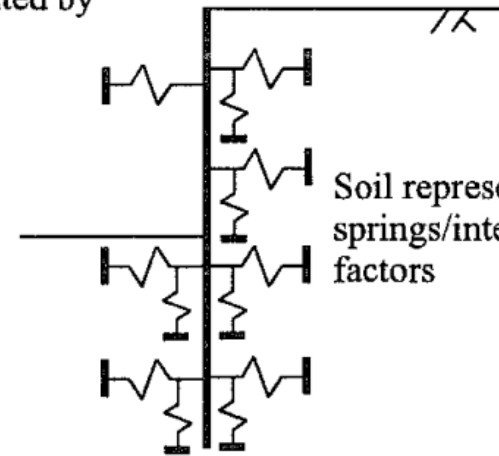
# Numerical Methods

## Beam Spring Approach



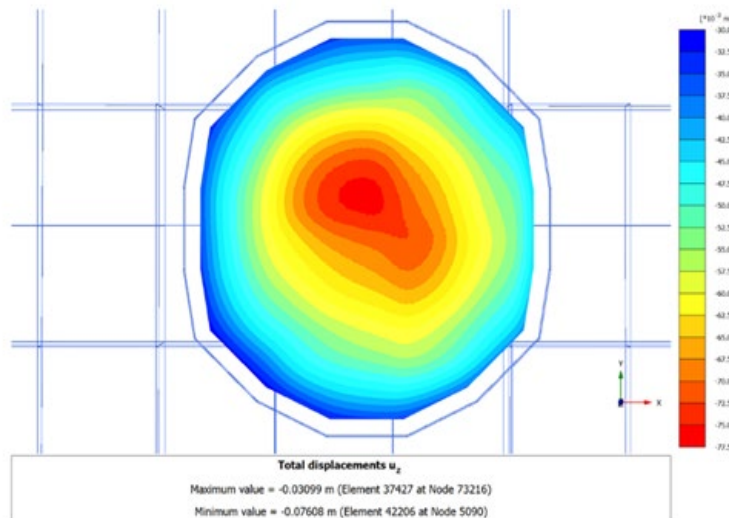
Soil represented by  
springs/interaction  
factors

Props/anchors  
represented by  
springs



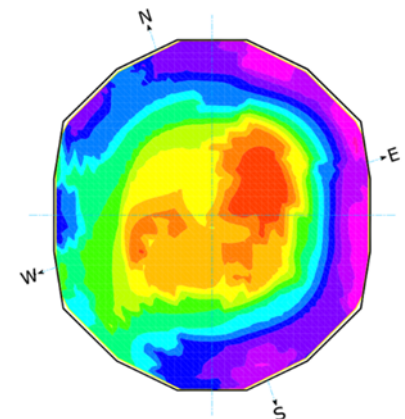
Soil represented by  
springs/interaction  
factors

*Settlements*



*Subgrade Moduli*

Number	From	To	Color
1	0.000000	5000.000	Red
2	5000.000	10000.000	Orange
3	10000.000	15000.000	Yellow
4	15000.000	20000.000	Light Green
5	20000.000	25000.000	Green
6	25000.000	30000.000	Light Blue
7	30000.000	35000.000	Blue
8	35000.000	40000.000	Dark Blue
9	40000.000	45000.000	Very Dark Blue
10	45000.000	50000.000	Black
11	50000.000	55000.000	Black
12	55000.000	60000.000	Black
13	60000.000	65000.000	Black
14	65000.000	70000.000	Black

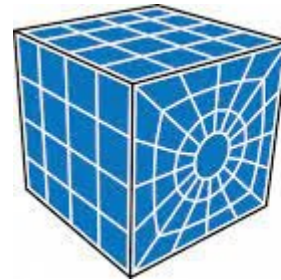


# Full Numerical Analysis

- Finite Difference



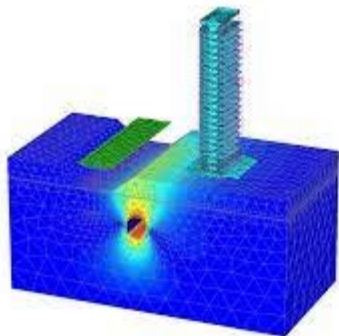
ITASCA™



FLAC3D™

- Finite Elements

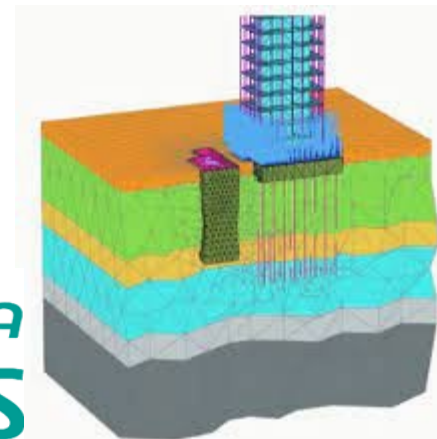
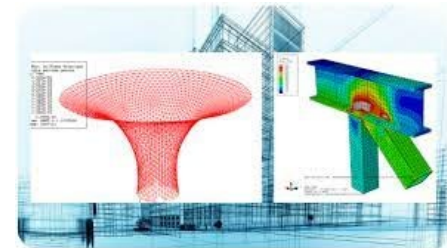
PLAXIS



SAP2000

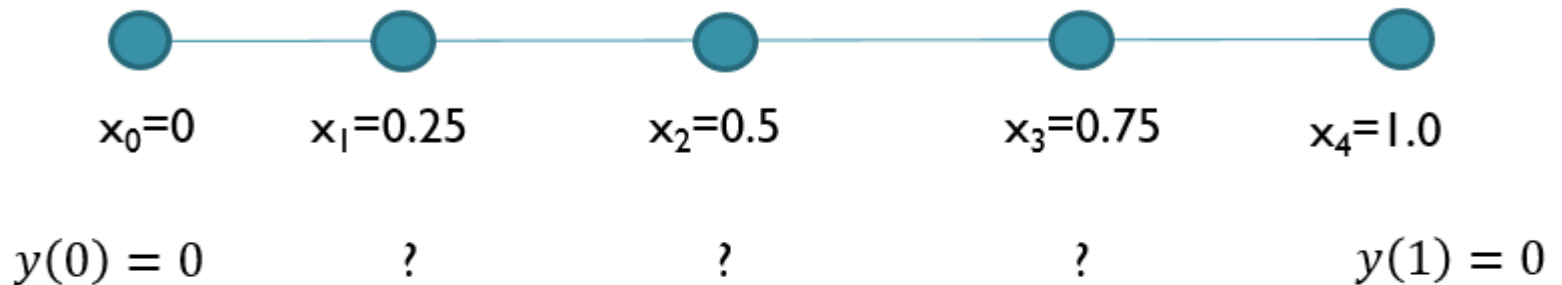


The logo for SIMULIA ABAQUS, featuring a stylized 'S' symbol followed by the text 'SIMULIA' and 'ABAQUS' in a bold, sans-serif font.



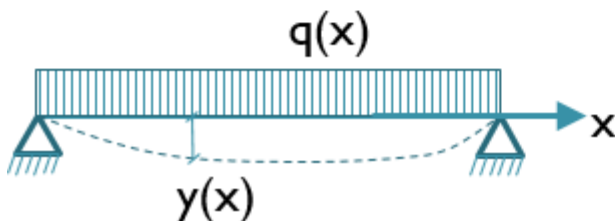
# Finite Difference

$$-EI y''(x) = M(x)$$



Using central difference formula for second derivative where  $i$  goes from 1 to 3

$$\frac{-y_{i-1} + 2y_i - y_{i+1}}{h^2} = \frac{1}{EI} M(x)$$

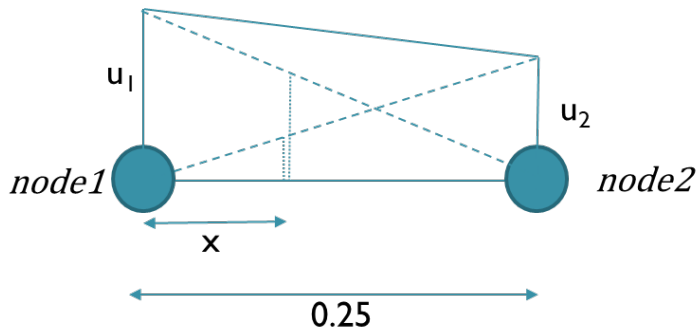


For a constant  $q(x)$  on a beam of  $L=1$

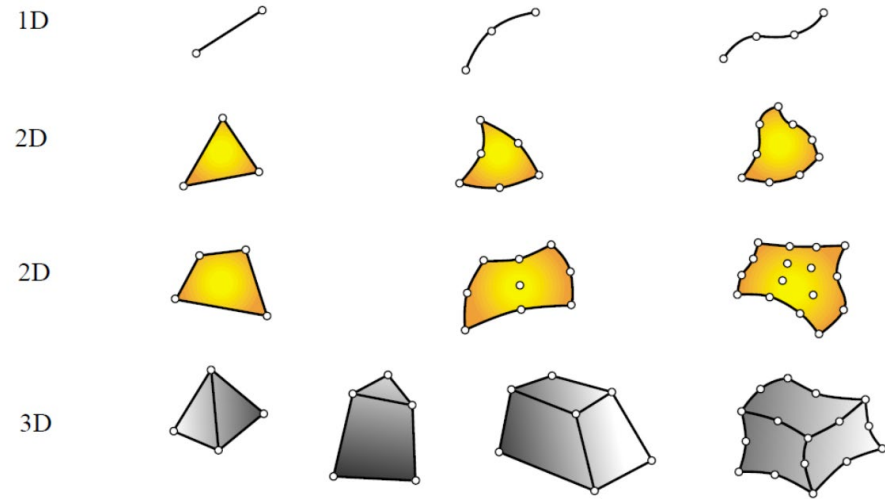
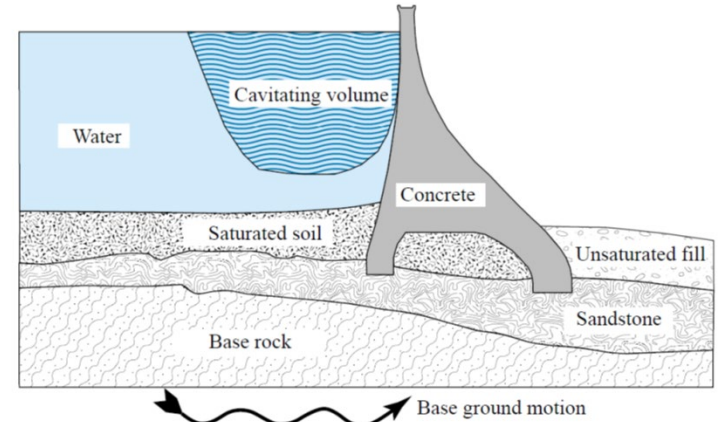
$$M(x) = \frac{1}{2} qx - \frac{1}{2} qx^2$$



# Analysis of a continuum

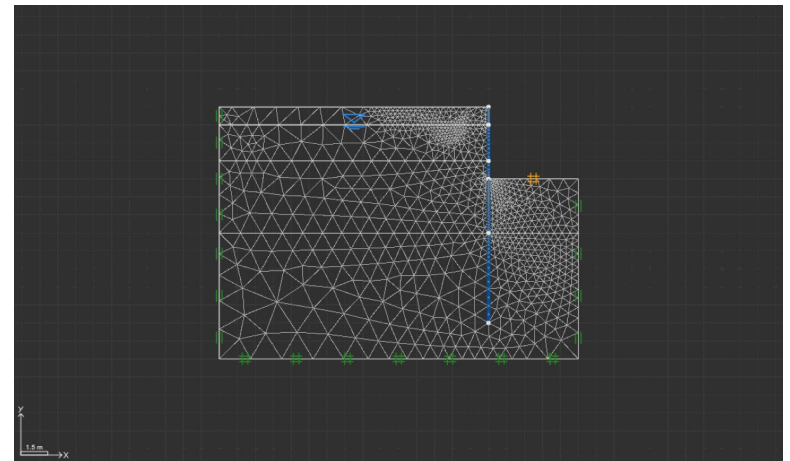


$$u_x = \left( \frac{0.25 - x}{0.25} \right) u_1 + \left( \frac{x}{0.25} \right) u_2$$



# Finite Element Limit Analysis

- Scott Sloan (2010)
- Optum GE software
- Searching for the maximum lower bound and the minimum upper bound by linear programming



# Solution Requirements

METHOD OF ANALYSIS		SOLUTION REQUIREMENTS				
		Equilibrium	Compatibility	Constitutive behaviour	Boundary conditions	
					Force	Disp
Closed form		S	S	Linear elastic	S	S
Limit equilibrium		S	NS	Rigid with a failure criterion	S	NS
Stress field		S	NS	Rigid with a failure criterion	S	NS
Limit analysis	Lower bound	S	NS	Ideal plasticity with associated flow rule	S	NS
	Upper bound	NS	S		NS	S
Beam-Spring approaches		S	S	Soil modelled by springs or elastic interaction factors	S	S
Full Numerical analysis		S	S	Any	S	S

S - Satisfied; NS - Not Satisfied

# Comparison: Design Requirements

**Table 2. Design requirements satisfied by the various methods of analysis**

Method of analysis		Design requirements		
		Stability	Movements	Adjacent structures
Closed form (linear-elastic)		No	Yes	Yes
Limit equilibrium		Yes	No	No
Stress field		Yes	No	No
Limit analysis	Lower bound	Yes	No	No
	Upper bound	Yes	Crude estimate	No
Full numerical analysis		Yes	Yes	Yes

Potts, D. M. (2003). Numerical analysis: a virtual dream or practical reality?. *Géotechnique*, 53(6), 535-573.

# Advantages of Numerical Analysis

- 1- Complicated and non-linear soil behavior (effect of time dependence, pore pressure migration)
- 2- Construction sequence
- 3- Complicated soil structure interaction problems (adjacent structures, interconnection with structure components)

# Challenges of Numerical Analysis

1- You have to be familiar with the constitutive model

2- You have to be familiar with the algorithms used to solve non-linear problems.

3- You have to be familiar with the software and how components are defined and the interaction between them.



**Thank you**